



Investigation of potential distribution on a CFRP coupon under impulse current. Test results and FDTD simulation.

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Abstract — CFRP is becoming in an important material for the future blades due to alternative renewable energy industry plans to increase the length of the blades. This work shows some analytical results about potential distribution on a CFRP coupon obtained after applying an impulse current with different rise time. Effects around electrodes are, symmetry behavior and some interesting comments about the influence of the rise time appear. A FDTD simulation is done and a comparison between FDTD and analytical results. The aim is to evaluate how useful can be this technique when current distribution is over an anisotropic material since tests are not always possible.

Keywords- lightning; wind turbines; blades; CFRP; FDTD; modelling

I. INTRODUCTION

Nowadays, the challenge of reducing the cost of alternative renewable energy [1] give rise to an optimization of the wind turbine performance. The best way to increase the wind energy production is to increase the swept area of the rotor by increasing the blade length. Modern wind turbines can reach altitudes of about to 200 m even higher in the near future [2]. Then blades length can exceed 80 m especially in offshore wind farm. In this scenario carbon fiber reinforced plastic (CFRP) becomes more relevant in blade manufacturing.

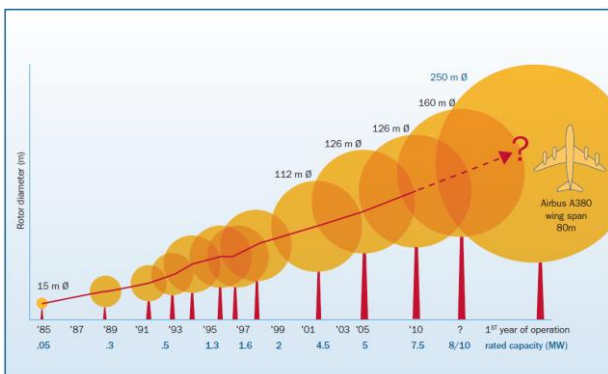


Figure 1. Evolution of wind turbines (adopted from [2]).

On the other hand, lightning protection system (LPS) in wind turbines is a very complex task and blades require a special attention because they constitute the most lightning-sensitive part of a wind turbine. Materials to build the blade, size of them and their rotating speed get complicated their lightning protection [3-4]. Lightning protection of wind turbines is covered by the IEC 61400-24 standard [5], although the continuous changings in wind turbines manufacturing force a constant review of it.

In this way, impulse current tests [6] are required to verify current distribution through the different conductive part of blades (down conductors, connection components and CFRP) and how it can affect to the damage mechanisms in blades. Electrical connections between LPS and CFRP elements require an especial attention taking into account the difficulty to do it. In this context, it is becoming more important a deep knowledge about electrical behavior of CFRP. In the last years some, works about this topic has been presented [6-10] but mostly under direct current and sometimes looking for damage identification [11-13].

Due to the complexity of real test over full size blades, increasingly is more necessary simulation tools to obtain accurate results of our designs. The finite different time domain (FDTD) method is an accurate way of resolving Maxwell's equations since Yee presented it in 1966 [14]. This kind of method is able to work at high frequency and take into account all the electromagnetic properties of the materials involved in a concrete performance, becoming a perfect tool to analyze the transient magnetic fields and voltages induced over a wind turbine [15-16] or in the body of an aircraft stroked by a lightning [17]. Among all the methods to solve Maxwell's equations, FDTD is the technique that continues growing due to the availability of numerical codes and increased computer capabilities.

This paper presents some tests under impulse current with different waveform. Taking as a reference the results obtained in a previous current distribution research [6], which it was observed that the current through CFRP had faster rise time than the current through down conductor of the LPS. For this reason, it is essential to analyze the behavior of the CFRP material under different waveform, in order to observe how the current was distributed. Some FDTD simulation are shown, trying to improve model tools because they can help the research with this composite anisotropic materials.

II. POTENTIAL MEASUREMENT ON THE COUPON

A. Test performance

For this work, a CFRP unidirectional ply sample is used with identical electrical characteristics to the sample tested in [7]. The configuration of the CFRP coupon and the electrodes are shown in the next figure:

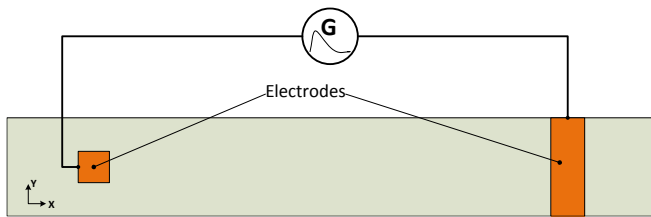


Figure 2. Configuration of CFRP coupon under test Geometry of the CFRP coupon and the electrodes. This view corresponds to the electrodes side. X-axis correspond to the carbon fibers direction.

The CFRP coupon is 725 mm length, 110 mm width and 2.62 mm thickness. The electrodes location are not just in the corners of the CFRP coupon, like real full size blades.

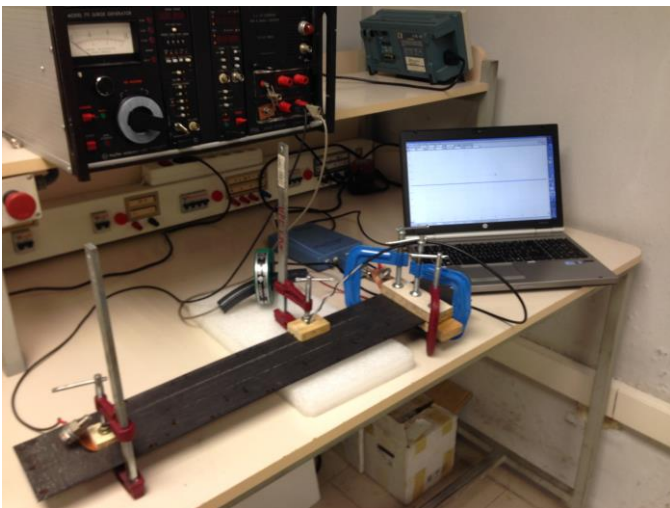


Figure 3. Test Performance. CFRP coupon connected to an impulse generator with the measurement system (digital recorder, current monitor and voltage probe).

In the same way, full size blades have not uniform width of CFRP along it. Trying to reproduce this situation, electrodes with different size is used with the idea of observing the behavior around the electrodes. The reference electrode

covered the full coupon width (110 mm), while the injection electrode was 35 mm square and it is connected at the half of the width of the coupon. The free distance between electrodes is 495 mm. C-clamps is used to fix the electrodes meanwhile an impulse current is applied. Over this sample, some different rise times were applied trying to observe potential distributions over the CFRP. Peak current was almost constant for each rise time waveform.

Potential measurement over CFRP coupon surface is not a trivial task due to the stray inductance effect of the measurement circuit especially when an impulse current is injected. For measuring the current through the coupon, it was used a Pearson 110A current monitor (CM). In the case of the voltage measured, it was performed a probe with two small electrodes with a 30 mm separation distance and the leads with a minimum distance over the surface, minimizing the stray inductance effect. A USB digital recorder (DR) was used to record the current and voltage signals. PicoScope 4424 digital recorder was used. It has 12 bits and a bandwidth of 20 MHz.

B. Experiment procedure

Taking as a reference the line along the half of the width of the coupon (line A), two more line were selected on both sides of line A and they were separated from it 30 mm (the distance between voltage probe electrodes). Line B and C were out of the influence of the injection electrode. Along these lines some points were selected to measure voltage. Voltage names were V_{ABx} (AB indicates the lines between the voltage was measured and x indicates the number of the point measured).

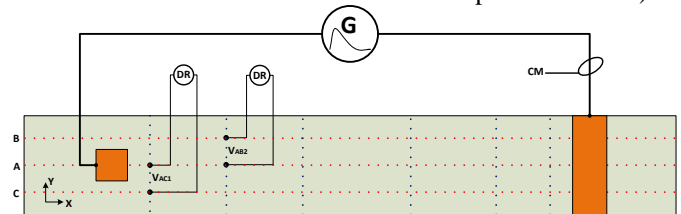


Figure 4. Measure of V_{ABx} and V_{ACx} voltages. Red lines shows the lines between the voltage were measured and blue lines represents the point of the measurement. Impulse current injected to the CFRP coupon in simultaneously measured with the digital recorder (DR).

In addition to V_{ABx} and V_{ACx} voltage measures, some voltages along line A were measured too. These voltages were called V_{AAx} (AA indicates that the voltage was measured over line A and x indicates the number of the point measured)

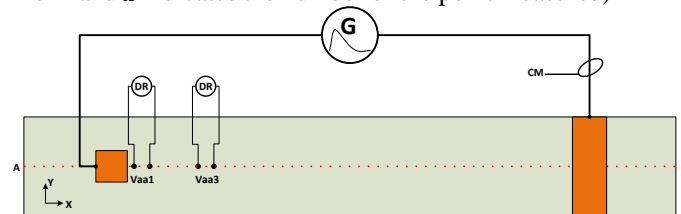


Figure 5. Measure of V_{AAx} voltages. Impulse current injected to the CFRP coupon in simultaneously measured with the digital recorder (DR).

The aim of this measurement were to observe the symmetry in CFRP behavior. The connection between CFRP and the impulse current generator was not realized in the middle of the material, as it is in a real full blade connection between the down conductor of the LPS and the CFRP connection. In the same way, in DC test was observed that almost all current applied to the injection electrode was conducted through fibers in front of this electrode and fibers out of this area were not effective for the current conduction. This phenomena was clearly observed with thermal images. The idea was to determine if, with impulse current, the behavior of the CFRP were the same or not.

C. Slow rise time impulse current

In this case, an impulse current with around 13 μs rise time was applied. The peak value of the injected current was 280 A and it was almost constant during measurements. Voltage and injected current were simultaneously measured at points indicated before.

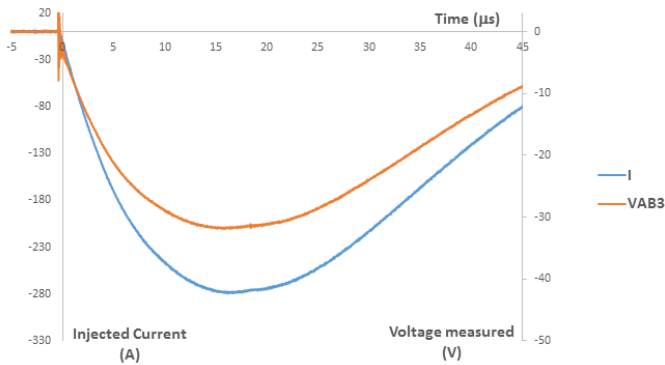


Figure 6. Example of injected current and voltage measured (V_{AB3}).

Next table shows the impulse resistance in all points measured. It was calculated dividing peak voltage by current.

TABLE I. IMPULSE RESISTANCE FOR ALL AB AND AC POINTS MEASURED

Position (mm)	Voltage name	Z_P (Ω)
x = 140	V_{AB1}	0.200
x = 140	V_{AC1}	0.207
x = 225	V_{AB2}	0.159
x = 225	V_{AC2}	0.148
x = 310	V_{AB3}	0.114
x = 310	V_{AC3}	0.113
x = 430	V_{AB4}	0.101
x = 430	V_{AC4}	0.086
x = 525	V_{AB5}	0.064
x = 525	V_{AC5}	0.057
x = 585	V_{AB6}	0.030
x = 585	V_{AC6}	0.031

TABLE II. IMPULSE RESISTANCE FOR ALL AA POINTS MEASURED

Position (mm) ^a	Voltage name	Z_P (Ω)
x = 125	V_{AA1}	0.018
x = 200	V_{AA2}	0.010
x = 230	V_{AA3}	0.009
x = 330	V_{AA4}	0.009
x = 425	V_{AA5}	0.010
x = 505	V_{AA6}	0.012
x = 575	V_{AA7}	0.017

a. Position indicates the coordinates of the positive probe electrode. The negative probe electrode was 30 mm separated in the same line.

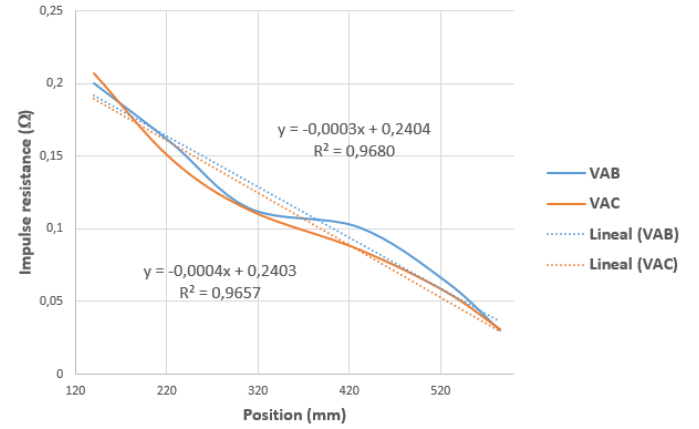


Figure 7. Potential V_{ABX} and V_{ACX} along the CFRP coupon with a slow rise time impulse current.

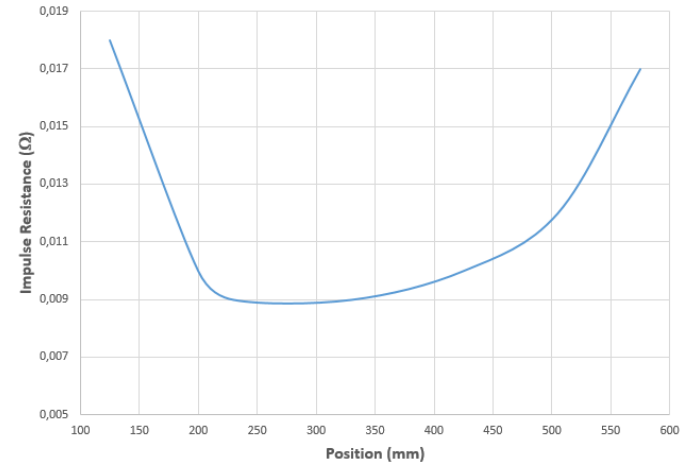


Figure 8. Potential V_{AAX} along the CFRP coupon with a slow rise time impulse current.

D. Fast rise time impulse current

In this case, an impulse current with around 3 μs rise time was applied. The peak value of the injected current was 460 A and it was almost constant during measurements. Voltage and injected current were simultaneously measured at points indicated before.

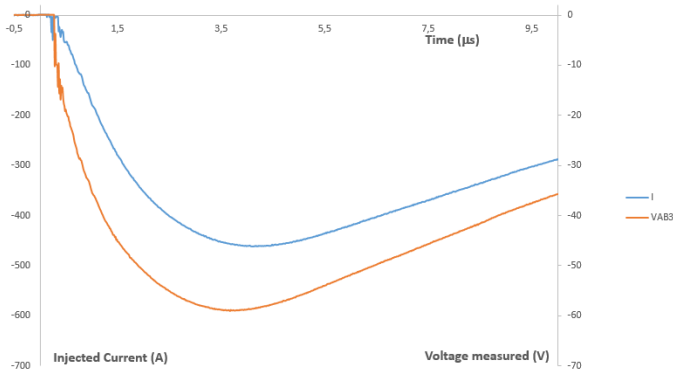


Figure 9. Example of injected current and voltage measured (V_{AB3}).

Next table shows the impulse resistance in all points measured. It was calculated dividing peak voltage by peak current. Figure 7 shows a delay between voltage and current that it didn't appear with slow rise time. It was not taken into account for the impulse resistance.

In the following table, it can be observed the impulse resistance in all points measured. It was calculated dividing peak voltage by peak current.

TABLE III. IMPULSE RESISTANCE FOR ALL AB AND AC POINTS MEASURED

Position (mm)	Voltage name	Z_P (Ω)
x = 140	V_{AB1}	0.190
x = 140	V_{AC1}	0.207
x = 225	V_{AB2}	0.160
x = 225	V_{AC2}	0.162
x = 310	V_{AB3}	0.128
x = 310	V_{AC3}	0.133
x = 430	V_{AB4}	0.094
x = 430	V_{AC4}	0.094
x = 525	V_{AB5}	0.056
x = 525	V_{AC5}	0.052
x = 585	V_{AB6}	0.028
x = 585	V_{AC6}	0.036

TABLE IV. IMPULSE RESISTANCE FOR ALL AA POINTS MEASURED

Position (mm) ^a	Voltage name	Z_P (Ω)
x = 125	V_{AA1}	0.234
x = 200	V_{AA2}	0.116
x = 230	V_{AA3}	0.100
x = 330	V_{AA4}	0.101
x = 425	V_{AA5}	0.098
x = 505	V_{AA6}	0.129
x = 575	V_{AA7}	0.145

a. Position indicates the coordinates of the positive probe electrode. The negative probe electrode was 30 mm separated in the same line.

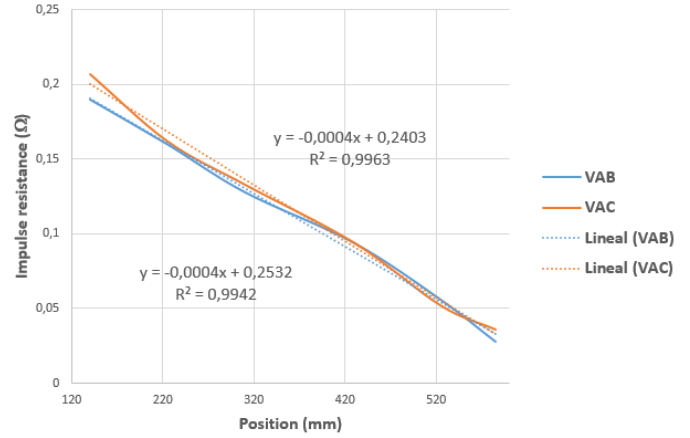


Figure 10. Potential V_{ABx} and V_{ACx} along the CFRP coupon with a fast rise time impulse current.

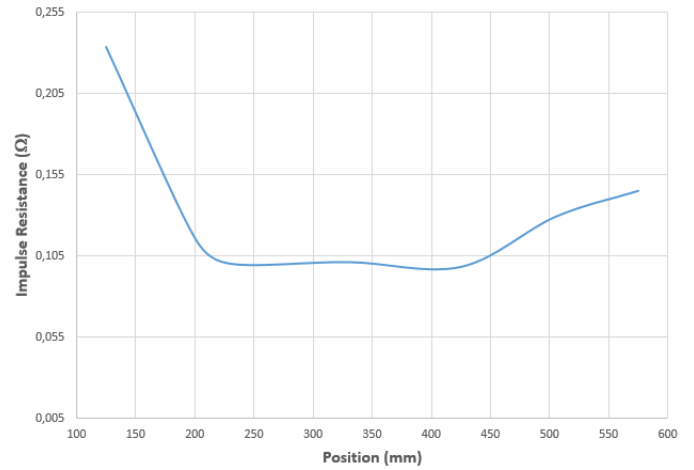


Figure 11. Potential V_{AAx} along the CFRP coupon with a fast rise time impulse current.

E. Discussion about results

After the results analysis, some interesting things could be observed. First of all, results show symmetric behavior, impulse resistance in both sides are very similar. Furthermore, impulse resistance in these points along CFRP coupon are almost equal, whereas with slower rise time is not as linear as faster rise time.

On the other hand, around the electrodes, potential concentration is more intensive than in the middle of the CFRP. Similar results were obtained with DC [7], although in this occasion, when the results from the different rise time were compared, a different behavior was observed. With a faster rise time, the potential concentration near reference electrode seems lower than slower rise time. Near injection electrode similar behavior appears. This trend should be analyzed specifically with more measurements around the electrodes.

Results show similar values for impulse resistance between AB lines and AC lines for all points and for both waveforms. For impulse resistance over line A (where greater part of the

injected current go through), the values are very different if the data from the two waveforms are compared. It indicates different effective conduction area depending of the rise time or the current density.

Another important result is the observation of the delay between the potential and the current injected for faster rise time while for slower rise time resistive behavior prevail. This delay should be more investigated even the stray inductance effect of the measurement system was minimize.

The anisotropic behavior of CFRP and the irregularities in the fabrication of the coupon could justify these results but more test should be done. Contact resistance has not been taken into account in this work.

III. FDTD SIMULATIONS

A. Simulation performance

Different parameters have been taken into consideration to carry on the FDTD modelling. First of all, the following values have introduced for the scale of the analytical space: 0.18 m x 0.074 m x 0.01 m. This space was divided into 1e-3 cubic cells.

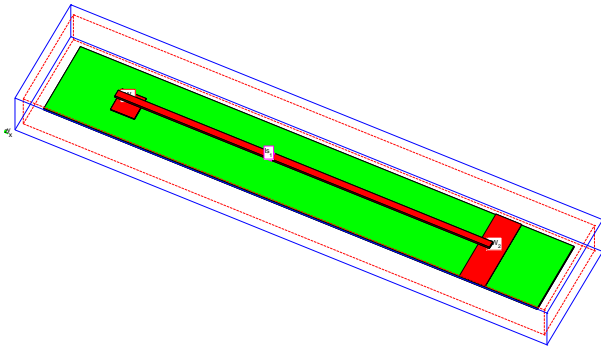


Figure 12. Geometry of the model

Secondly, to achieve the 2 μs rise time with the dimension of the unit cells determined before, it was required a number of time steps of 384000.

Finally, this simulation required a CPML (Convolutional Perfectly Matched Layer) boundaries, because the standard ones were shown to be ineffective for absorbing evanescent waves [18]. For this reason, this other kind of boundaries were implemented according to the following settings: air buffer boundary with 20 cells in each side of the model and 8 cells of CPML boundaries.

B. Results and discussion

First of all, result of current density distribution from the FDTD simulation is showed. It shows how the current spreads from the injection current to the reference current. Potential

distribution around the electrodes could be analyzed from these simulations but they need real test to validate the results.

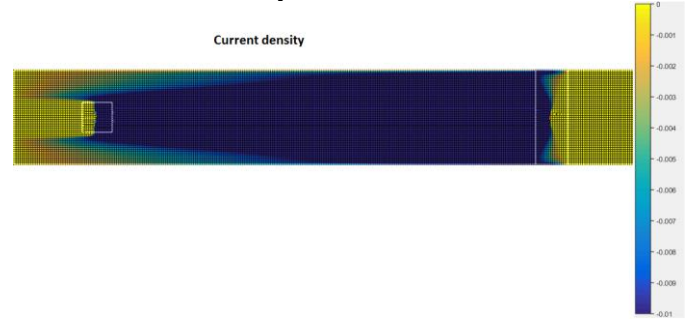


Figure 13. Current density on CFRP coupon obtained from FDTD simulation.

Similar data was obtained from FDTD simulation to compare them with data obtain from the tests. Injected impulse current and potential could be calculated.

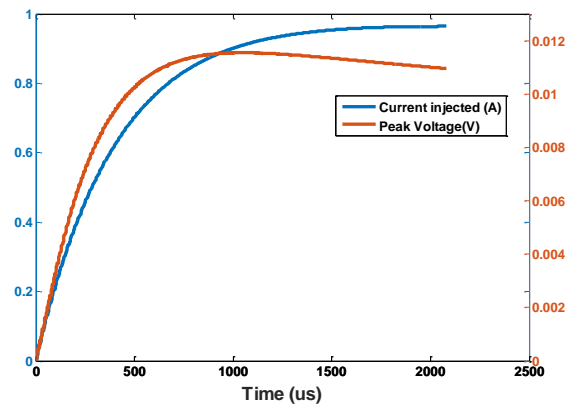


Figure 14. Example of injected current and voltage measurement from FDTD simulation.

Figure 14 shows a delay between voltage and injected current like measurement obtained from faster rise time and it may indicated that this delay is not introduced from the measurement system.

TABLE V. IMPULSSE RESISTANCE FOR ALL AB POINTS MEASURED

Position (mm)	Voltage name	Z _P (Ω)
x = 140	V _{AB1}	0.037
x = 225	V _{AB2}	0.025
x = 310	V _{AB3}	0.018
x = 525	V _{AB5}	0,005

TABLE VI. IMPULSSE RESISTANCE FOR ALL AA POINTS MEASURED

Position (mm) ^a	Voltage name	Z _P (mΩ)
x = 125	V _{AA1}	5.85
x = 225	V _{AA2}	4.94
x = 430	V _{AA3}	4.09
x = 525	V _{AA4}	4.14

a. Position indicates the coordinates of the positive probe electrode. The negative probe electrode was 30 mm separated in the same line.

V_{ACx} voltages are not showed on TABLE V because are the same than V_{ABx} voltages due to the symmetry of the model.

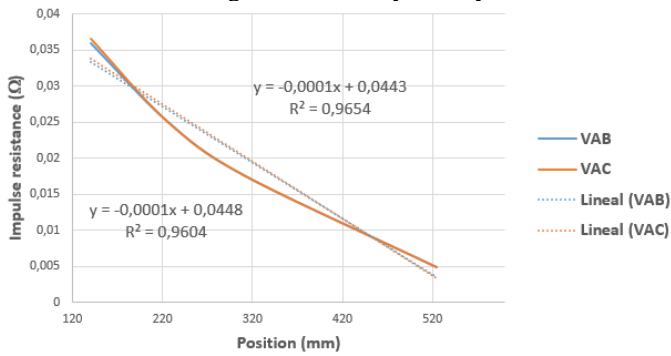


Figure 15. Potential V_{ABx} and V_{ACx} along the CFRP coupon obtained from FDTD simulation.

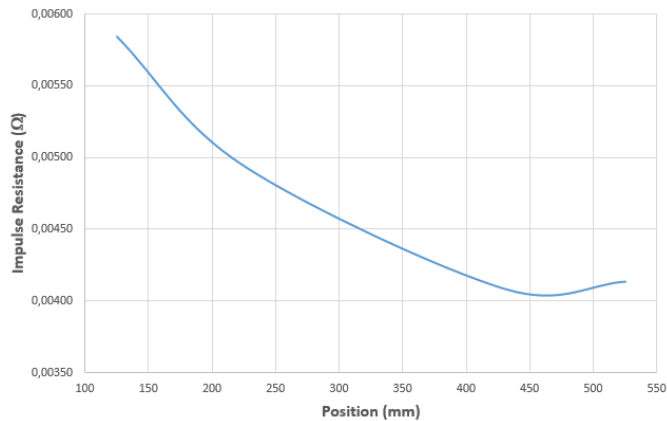


Figure 16. Potential V_{max} along the CFRP coupon with a fast rise time impulse current.

Although in this case, potential concentration around electrodes are not as evidence than analytical results some similarities can be observed. More points should be calculated to improve the graphic.

IV. CONCLUSIONS

In this paper, it was obtained the surface potentials for impulse current with different rise time in a CFRP coupon. Symmetry behavior in the fibers direction and near the electrodes were analyzed. Different behaviors around electrodes were observed when the rise time of the impulse current increased. In addition to this, a delay between voltage and current injected was observed when the rise time of the impulse current increased. This delay appear in the FDTD simulation too. FDTD could be an important tool to help the research work in this area. All the results presented could be useful for lightning protection of CFRP in wind turbine but some more test and measurements should be done to delve into in the CFRP behavior knowledge.

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